

NOAA Technical Memorandum EDS CEDDA-2



CHARACTERISTICS OF THE LOWER ATMOSPHERE NEAR SAIPAN, APRIL 29 TO MAY 16, 1945

Joshua Z. Holland

Washington, D.C. April 1975

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#### PREFACE

The report presented herein was transmitted to the Headquarters, U.S. Army Air Forces Weather Service, Pacific Ocean Area, on June 11, 1945. It was prepared by me, based on a field program carried out with the assistance of Lt. Earl Sargent of the U.S. Army Air Force. It is the meteorological part of an investigation under the direction of D. E. Kerr of the MIT Radiation Laboratory. The overall investigation had to do with factors affecting the performance of a radar on Saipan. The report was originally classified "Confidential." I have been encouraged to publish the meteorological part, even at this late date, because of the recent increase of interest in the atmospheric boundary layer over the tropical ocean and because data of this kind that are available are still largely limited to the Atlantic and Caribbean areas. It is interesting to see that the structure found over the western Pacific Ocean is identical to that found over the western Atlantic, despite considerable differences in observational technique.

I had considered reworking this material to condense it and to overcome some slight quaintness of notation and terminology. However, I have become convinced that it will be quite satisfactory from the standpoint of readability, and highly desirable from the standpoint of avoiding further delays in its "seeing the light of day," to present the report exactly in its original form except for addition of a few explanatory footnotes and the elimination of two final sections containing suggested extensions and recommendations that were not an essential part of the research and are no longer of interest.

Joshua Z. Holland August 1973

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## CHARACTERISTICS OF THE LOWER ATMOSPHERE NEAR SAIPAN, APRIL 29 TO MAY 16, 1945

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Abstract. This is the meteorological part of a World War II investigation of the performance of a U.S. Army search radar located on Saipan in the Marianas Islands. Thirty detailed temperature and humidity soundings of the lowest 10,000 ft over the ocean were made with a mercurial psychrometer aboard a PBY flying boat. The data are analyzed to show typical characteristics of the vertical structure. The existence of a layer of strong gradient of M (the modified index of refraction) between the lowest level sampled (20 to 30 ft) and the surface is inferred. A layer of nearly constant potential temperature and mixing ratio is generally found extending up to an altitude that averages 1,700 ft and ranges from 1,000 to 2,600 ft. This moist "stirred layer" is generally topped by a stable transition layer. Above this a drier layer with a temperature lapse rate between dry and moist adiabatic, containing cumulus clouds, extends up to a second stable layer, the "trade inversion." Seven of the 12 aircraft soundings that reached 8,000 ft, and 16 out of 21 radiosonde observations taken at Saipan during this period, showed such a stable layer with an average base altitude of 5,000 ft.

#### 1. GENERAL

## 1.1 Objectives

The objectives of the present study are as follows:

- (1) To make detailed low-level meteorological soundings in the vicinity of Saipan; to analyze these soundings in terms of the distribution of the "modified index of refraction," and to determine the effect of meteorological factors on the coverage of the AN/CPS-1 radar on Mt. Tapotchau, Saipan.
- (2) To suggest (a) significant meteorological factors to be looked for in similar studies in other locations, such as Iwo Jima and Okinawa; (b) requirements for such investigations; and (c) suitable methods for conducting such investigations.

## 1.2 Description of Investigation

The 30 airplane soundings discussed here were made during the period April 29 to May 16, 1945. The instrument used for measuring temperature and humidity was a mercurial psychrometer, constructed at the MIT Radiation Laboratory, and installed on the top of the nose of a PBY flying boat, well forward of the engines. A radiation shield was constructed out of two fruit cans with the flat ends removed, joined end to end. The thermometer bulbs were protected by the shield from direct illumination by the sun, but it is possible that the readings were influenced somewhat by reflected radiation from the inner surface of the shield. No correction was made for this effect. Two observers were required for the soundings. One observer read the psychrometer, while the other read the pressure altimeter and airspeed indicator and recorded all data. 1 Temperatures were read to the nearest 0.1°C. After several unsuccessful attempts at determining the dynamic temperature correction by flying at different airspeeds at a constant altitude and plotting temperature readings as a function of airspeed, the correction  $0.8(v/100)^2$  (which appeared to be a reasonable value and where v = airspeed, probably in knots) was added to both temperature and wet-bulb temperature readings. Soundings were made to the northeast and east of Saipan (where air traffic was very light) at varying distances from the island. Most soundings were within 100 mi of Saipan, but on May 9 soundings were made 50, 100, and 150 mi east of Saipan, in order to study the horizontal variations of the M-distribution<sup>2</sup> over the entire radar range. All the soundings have been included in the averages, because they are considered to be equally representative of the climate. No sea-surface temperatures were measured directly, but were extrapolated from the dry-adiabatic lapse rate in the stirred layer. No significant variation in these sea-surface temperatures was noted. Soundings were made around midday and early afternoon, and mostly in relatively good weather. Only on May 4 and 14 were flights made in showery weather. Of the 30 soundings, 25 reached 4,000 ft and 12 exceeded 8,000 ft.

The other data used to complete the picture include the Saipan radiosonde, winds-aloft (rawinsonde) and surface observations. The radiosonde data were obtained from the original records at Kagman Point Upper Air Section, Saipan, where more levels are recorded than are transmitted in the final message, and temperatures are recorded to the nearest 0.1°C. Although the radiosonde record is unsuitable for detailed analysis of the lower 2,000 ft, it agrees well with the psychrometer observations in the middle layer (approximately 2,000 to 4,000 ft), particularly in moisture content. The complete set of observations makes a self-consistent picture, possibly not quantitatively representative of the entire season, but probably a reasonably good sample.

<sup>&</sup>lt;sup>1</sup>The soundings were of the "stepped" type. Each reading was taken on a straight and level leg of a 1- or 2-min duration--long enough to allow the psychrometer to approach equilibrium.

 $<sup>^{2}</sup>$ The definition of M is given in the following section.

#### 2. SUMMARY OF ATMOSPHERIC CHARACTERISTICS

## 2.1 Description of Model of the Lower Atmosphere

From an examination of the airplane and radiosonde soundings, it became apparent that the structure of the lower atmosphere is characterized by the following features:

- (1) There is a lower stirred layer in which the potential temperature and mixing ratio are uniformly distributed with height and in which the water vapor is unsaturated at the surface. The potential temperature and mixing ratio are nearly constant from day to day.
- (2) At the top of the stirred layer there is a stable transition zone, frequently showing a small temperature inversion. In this zone the mixing ratio drops off more or less abruptly with height. The mixing-ratio lapse rate is greatest in the clear spaces between clouds, and least within the cumulus clouds. The temperature inversion, likewise, is most marked in the clear spaces between clouds, and absent within the air columns containing the clouds.
- (3) Above this transition zone there is a layer of intermediate moisture content which shows a slow decrease with height, and varies appreciably between cloud and clear spaces. The temperature lapse rate in this layer is usually between the moist and dry adiabatic, but is sometimes less than the moist adiabatic.
- (4) At the top of this intermediate layer, there is usually a second stable layer, in which the mixing ratio shows a more rapid decrease with height. The air above this second transition layer is dry upper air. Frequently this inversion disappears (or is displaced to a much higher level), and then the intermediate mixing ratios extend to abnormally great heights. This second inversion is the upper limit of general low cloud development, but may be penetrated by individual towering cumuli.

## 2.2 Characteristic Quantities

Selected characteristic quantities for each sounding, together with maximum, minimum, and average observed values of each characteristic quantity, are contained in table 1 (airplane soundings) and table 2 (radiosondes). The average values are used in the construction of figure 1.

The following data are obtained from an analysis of the airplane observations. The Saipan radiosonde was too much influenced by surface heating, cooling, and frictional stirring, and lacking in sufficient detail for use in evaluating most of these features.

(1)  $\theta_{\text{st}}$ : The potential temperature of the stirred layer. This was obtained by drawing the best dry-adiabat through the plotted temperatures in the stirred layer, and assuming a surface pressure of 1,013 mb.

- (2)  $T_s$ : The temperature of the intersection of the  $\theta_{st}$  line with the 1,013-mb isobar. Assuming neutral thermal equilibrium, this is equal to the sea-surface temperature. This assumption appears justified in view of the following considerations:
- (a) The known horizontal homogeneity of the sea-surface temperature in this region, and the long trajectory of the air over a uniform water surface.
- (b) The absence of any observed stable or superadiabatic temperature lapse rates near the sea surface during the course of these flights.
- (c) The near-constancy of  $\boldsymbol{\theta}_{\text{st}}$  from day to day under various weather conditions.
- (3) w: The saturation mixing ratio corresponding to T at 1,013 mb. This is the mixing ratio in the air immediately adjacent to the sea surface.
- (4)  $\overline{w}_{st}$ : The average value of the mixing ratio in the stirred layer. Although w was nearly constant in each sounding, it varied more from one sounding to another than did  $\theta_{st}$ . In some cases a scattering of values of w about the mean was obtained in the stirred layer.
- (5)  $\Delta M$ : The deficit of modified index of refraction<sup>3</sup> in the bottom of the stirred layer. This is equal to M<sub>S</sub> M<sub>S</sub> =  $79/T_S^2 \times 4,800$  (e<sub>S</sub> e<sub>S</sub>), where e<sub>St</sub> is the vapor pressure in the stirred layer measured at 1,013 mb atmospheric pressure.
- (6)  $H_1$ : The height of the top of the stirred layer. At this point  $\theta$  and w change abruptly with increasing height.
- (7)  $\rm H_{cl}$ : The measured height of the base of the low clouds. These heights were determined visually by the observer in the airplane at the moment of passage through the cloud level.
- (8)  $\Delta w_1$ : The decrease of mixing ratio through the transition layer at the top of the stirred layer. This is the difference between  $w_{st}$  and the value of w at the top of the narrow layer of rapid moisture decrease.
- (9)  $\Delta T_1$ : The change in temperature through the transition layer determined by  $\Delta w_1$ .
  - (10)  $\Delta h_1$ : The depth of the transition layer determined by  $\Delta w_1$ .
- (11)  $\Delta \text{M}_{1}\colon$  The change in modified index of refraction through the transition layer.

 $<sup>^3</sup>$ Modified index of refraction M = 79(P + 4,800e/T)/T + 0.0478h, where T = temperature in degrees centigrade, P = pressure in millibars, e = vapor pressure in millibars, and h = height in feet.

- (12)  $v_{20}$ : The windspeed at 2,000 ft, obtained from the Saipan rawinsondes.
- (13)  $\Delta T_{20-40}$ : The change in temperature from 2,000 to 4,000 ft. At the dry-adiabatic lapse rate,  $\Delta T_{20-40}$  = -6.1°C. At the saturated-adiabatic lapse rate,  $\Delta T_{20-40}$  = -2.6°C.
- (14)  $\overline{w}_{25-40}$ : The average mixing ratio in the layer from 2,500 to 4,000 ft. This is a measure of the moisture content of the intermediate layer. The lower limit was chosen so as always to be above the transition layer.
- (15) Weather (general): The prevailing weather conditions as observed from the airplane.
- (16) Weather (sounding): Actual weather phenomena encountered by the airplane during the sounding.

The following data are tabulated in table 2 for the Saipan radiosondes during the period from May 6, 1300 GMT, to May 16, 1300 GMT. The original records were used. Approximate values of  $\rm H_2$  and  $\rm \Delta h_2$  were obtained from plotted radiosonde soundings in AAF Weather Central, Guam, for the period April 28, 1300 GMT, to May 6, 0100 GMT, and are shown in the time cross section (fig. 2, facing page 20), but are not included in the averages.

- (1)  $\Delta T_{20-40}$ .
- (2)  $\overline{w}_{25-40}$ .
- (3) H<sub>2</sub>: The height of the base of the second stable layer. This zone appeared in 15 of the 21 radiosonde soundings. The approximate values obtained for the preceding week exceeded 6,000 ft in five cases. The average value obtained during the period covered by accurate radiosonde data may be abnormally low.
  - (4)  $\Delta w_2$ : The change in mixing ratio through the second stable layer.
  - (5)  $\Delta T_2$ : The change in temperature through the second stable layer.
  - (6)  $\Delta h_2$ : The depth of the second stable layer.
- (7) dT/dh<sub>100</sub>: The lapse rate in the layer just below 10,000 ft. The temperature at 10,000 ft and the temperature at the next point, at least 100 m lower, were used. The dry-adiabatic lapse rate is  $3.0^{\circ}$ C/1,000 ft, and the moist adiabatic is  $1.5^{\circ}$ C/1,000 ft.
  - (8)  $T_{100}$ : Temperature at 10,000 ft.
  - (9)  $W_{100}$ : Mixing ratio at 10,000 ft.

The following data are plotted in time sequence in figure 2 (facing p. 20):

- (1) Three-hourly Saipan surface observations, plotted according to the station model used in synoptic analysis.
- (2) Winds at 2,000 and 4,000 ft, from the Saipan rawinsonde observations.
  - (3) H<sub>1</sub> from airplane observations.
  - (4) H2 from Saipan radiosondes.
  - (5)  $H_{c1}$  from airplane and surface measurements.
- (6) Cloud and weather cross section based on airplane and surface observations.

### 3. FRICTIONAL BOUNDARY LAYER

#### 3.1 Theory

According to R. B. Montgomery (1944) under conditions of neutral thermal equilibrium between the frictionally stirred lower air and the sea surface, the water vapor at the base of the homogeneous stirred layer must be unsaturated. There is, then, a moisture deficit at the base of the stirred layer with respect to the saturated air immediately adjacent to the ocean surface. The shallow transition layer between the surface and the base of the homogeneous layer is known as the "frictional boundary layer." This layer has been shown by theory and observation to occupy roughly one-tenth of the "layer of frictional influence" that extends to the top of the stirred layer. The rapid transfer of water vapor upward through the boundary layer is compensated for by the loss of moisture to the relatively dry air above the stirred layer, both by mechanical stirring and by thermal convection. some cases of large vertical vapor-pressure gradients at the top of the stirred layer, molecular diffusion may play an appreciable role.) This dynamic equilibrium maintains a nearly constant mixing ratio in the stirred layer.

Within the frictional boundary layer, the windspeed, potential temperature, and mixing ratio vary logarithmically with height, according to the equation:

$$\frac{dq}{dln(h)} = \Gamma(q_S - q_b) ,$$

where  $q_b$  is a representative value of the quantity q at a height b, and  $q_S$  is the value of q at the sea surface. Since in the case of neutral equilibrium  $\theta_S=\theta_b$ ,  $d\theta/d\ln(h)=0$  in the boundary layer as well as in the remainder of the friction layer. Montgomery (1944) used  $\Gamma=0.08$  for b=50 ft to calculate the vertical distribution of the modified index of refraction, M, in the boundary layer. At first M decreases rapidly, then more slowly, until

dM/dh = 0 at the height d = 2 ft x  $\Delta M$ , where  $\Delta M$  is equal to M at the surface minus M in the stirred layer extrapolated linearly to the surface. The height d is known as the "duct height." When the sea-surface temperature and pressure are constant, AM is a function of Aw alone. Table 3 gives eg,  $w_s$  for varying values of  $T_s$ . Table 4 gives  $\Delta M$  as a function of  $\Delta w$  at  $T_s = 28$ °C. Mongomery's relation between d and  $\Delta M$  is admittedly oversimple and based on insufficient data (particularly for our purpose, since all his observations were made over middle-latitude coastal waters). Nevertheless, he ventures the estimate that the large vertical gradients of w and M will be confined to the lower 100 ft. With data obtained from the U.S. Weather Bureau Atlas of Climatic Charts of the Oceans (1938) he predicts that a permanent M-inversion extending to roughly 30 ft will be found in the Guam area. Both these statements are borne out by our measurements, although the average values of AM as given by the climatic charts are less than half the observed values (his charts showing  $\Delta M$  = 19 for March, April, and May and  $\Delta M = 21$  for June, July, and August).

The assumption of neutral thermal equilibrium is supported by the climatic charts, which show a temperature deficit of about 0.3°C for this region at 1300 GMT in March, April, and May. This is equal to the diurnal variation of the sea-surface temperature in the tropics, according to Sverdrup (1942), and probably somewhat less than the diurnal variation of the surface air temperature (Petterssen, 1940). Furthermore, Montgomery (1944) finds that the entire homogeneous layer will adjust to horizontal surface-temperature gradients of a degree or two in a few miles. It is very unlikely that stronger gradients exist in the open ocean in the vicinity of Saipan. All but one of 28 surface temperatures obtained by dry-adiabatic extrapolation from airplane observations in the stirred layer were within 0.3°C of the average value of 27.7°C, which agrees closely with the mean sea-surface temperature for this season. (The CINCPAC-CINCPOA Bulletin No. 4-45 gives, for the 5° square including Saipan, 81°F for April and 82°F for May; our average for April 28 to May 16 is 81.9°F.)

#### 3.2 Measurements

Although 14 of the 30 soundings discussed here include measurements below 30 ft, no definite large vertical gradient of potential temperature or mixing ratio appears at the base of any of the soundings. However, assuming neutral thermal equilibrium, large M-deficits were always found, the average value of  $\Delta M$  being 44 units. If d=2 ft x  $\Delta M$ , the M-inversion should have begun to appear at about 90 ft, with strong vertical gradients of w and M between 50 and 20 ft. It is evident that the approximation d=2 ft x  $\Delta M$  is not applicable in this area. T is dependent on wind velocity and stability, and the value 0.08 may be based on incorrect values for this climate. Nevertheless, it seems safe to conclude from our measurements that a very low, intense duct is always present. Montgomery's predicted duct height of 30 ft seems not unreasonable, but detailed measurements will be necessary before anything definite can be said about its structure.

## 3.3 Relation of $\Delta M_{S}$ to Other Characteristic Quantities

In spite of the lack of direct measurements of duct height, some idea of the probable variation of intensity of the surface duct can be obtained from the variation of  $\Delta M_S$ . The small variation of  $\Delta M$  may be related to some of the other characteristics of the lower atmosphere.

Since  $T_s$  is so nearly constant, it may be expected that  $\Delta M_s$  will be mainly dependent upon  $\Delta w_s$ , which in turn depends upon  $\overline{w}_st$ . Figure 3 shows the observed values of  $\Delta M_s$  plotted against the corresponding values of  $w_{st}$ . It is seen that the points generally fall within three M-units of the line  $\Delta M_s = 7(23.1 - \overline{w}_{st})$ . The value of 23.1 in this empirical equation is the surface value of  $w_st}$ , which agrees well with the average observed value of 23.0. Thus, in the vicinity of Saipan, in this season, it is only necessary to know the value of  $w_st}$  in the stirred layer in order to make an accurate estimate of the M-deficit.

The mixing ratio in the stirred layer  $(\overline{w}_{st})$  is related to the height of the turbulence inversion  $(H_1)$ . It is seen from figure 4 that the higher the mixing ratio, the lower is the inversion. The inversion usually occurs just below the condensation level, which varies with the mixing ratio, as described in section 4. We can conclude that the surface duct will be strongest when the cloud level and the turbulence inversion are highest.

The extent to which the stirred layer is distorted by local effects may be judged from the sounding on May 8, 1520 GMT. On this occasion, readings between 500 and 1,500 ft were taken over Saipan harbor, in the lee of the island. In this layer, the mixing ratio was 15.2, as compared with values greater than 16 in the lowest 500 ft and in other soundings made on the same day east of the island. This dry air had probably subsided from above the stirred layer after passing across the 1,500-ft ridge in the center of the island.

## 4. TURBULENCE INVERSION

#### 4.1 Theory

In a completely stirred layer the air mass is vertically homogeneous; that is, the mixing ratio and potential temperature are constant up to the condensation level, and change at the saturated rate above that level. If the stirred layer extended above the condensation level, an overcast would be present at that level. But since scattered cumulus clouds are usually observed rather than a low overcast, it may be inferred that the stirred layer does not reach the condensation level except in patches. Between the clouds there must be a stable layer that sets an upper limit for vertical stirring immediately below the condensation level. Furthermore, just as the frictional stirring results in a moisture deficit at the base of the homogeneous layer, it should also result in a moisture excess at the top of that layer, when compared with the unstirred (and probably descending) air between the cumulus clouds. This inversion will be absent in the air columns containing clouds. Between clouds, however, it may be strong enough to show a decrease of modified index with height.

Theoretically (Byers, 1944), the height of the layer of frictional influence, H, is proportional to the windspeed, and increases with increasing surface roughness and decreasing stability, temperature, and latitude. The roughness is expressed by a length Z, the roughness coefficient, which is believed to be about 1/30 the height of the roughness elements. The values of H in table 5 were obtained from Byers (1944), using latitude 15°. The temperature and stability values used in the construction of this table were not known, but were probably representative of middle-latitude conditions.

## 4.2 Measurements

A stable layer was found at the top of the homogeneous layer in every airplane sounding except those taken through clouds. The height (H1) and strength  $(\Delta w_1, \Delta T_1, \Delta h_1, \Delta M_1)$  for each sounding and the average for the series are given in table 1. The average structure of the H1 inversion is shown in figure 1. It is seen that the average height of the top of the stirred layer is 1,700 ft, which is 50 ft less than the average cloud height observed. Based at this height there is a stable layer whose average depth is 240 ft, in which the temperature drops only 0.1°C. The transition from the moist stirred layer to the relatively dry air above takes place mainly in this narrow layer, the mixing ratio showing an average drop of 2.0 g/kg from its average value of 16.8 in the stirred layer. In most cases a weak duct was present; the average decrease was 4 M-units. The strongest duct in this zone was observed on May 9, with a decrease of 20 M-units in 100 ft. This persistent duct, which ranged in height from 1,000 to 2,600 ft, might be expected to cause occasional super-refraction of radiation from a radar set located at 1,500 ft, particularly when the inversion is slightly lower and more intense than average.

In two cases (April 29, 1046 1.t., and May 12, 1445 1.t.) an inversion was found at the top of a layer of flat cumulus clouds. With these exceptions, all the observed M-inversions occurred in the clear spaces between clouds. In several cases, also, two inversions were found in the vicinity of the cloud base. Since both inversions frequently showed weak ducts, they were both included in the averages. It is possible that these soundings represent a transitional condition, and that each of the two inversions is the predominating one over a different area or period of time.

The measurements of the depth of the transition layer ( $\Delta h_1$ ) cannot be regarded as sufficiently accurate for refined gradient calculations, since of 31 values measured, 17 were between consecutive points in the sounding. The lower 55 percent of the  $\Delta h_1$  values, then, were determined by the spacing between readings, and might have been considerably smaller had more detailed measurements been made.

No clear indication of the height or strength of the  $\rm H_1$  inversion was found in the Saipan radiosonde soundings. Surface heating and cooling, as well as increased frictional stirring due to passage over land, cause great changes in the lower 2,000 ft. In any case, the radiosonde is not suitable for direct measurement of such fine vertical variations.

## 4.3 Related Atmospheric Characteristics

Wind Velocity. Windspeeds at 2,000 ft, as measured by the Saipan rawinsondes, varied from 2 to 19 mi/h at the times of the airplane soundings. The corresponding winds at 4,000 ft varied from 2 to 24 mi/h. No positive correlation appears to exist between windspeed and height of the  $\rm H_1$  inversion. From table 5 it would be expected that  $\rm H_1$  would vary from about 1,000 to 8,000 ft, but  $\rm H_1$  is lower and much more steady than this. However, the strongest winds were observed under conditions of strong convective activity (fig. 2), and probably do not represent the mean wind flow. The  $\rm H_1$  inversion was found to be lowest under these same weather conditions, as discussed more fully below. Since both strong winds and instability would be expected from the turbulence theory to raise rather than lower the inversion level, it may be concluded that this level is determined more by the strength of local subsidence associated with individual convective cells than by prevailing stability and windspeed.

Cloud Level. It was indicated in section 4.1 above that the prevalence of scattered cumulus clouds rather than a low overcast suggested the presence of an inversion just below the condensation level. It was also noted in section 3.3 that the higher the mixing ratio, the lower is the turbulence inversion. The adiabatic condensation level, then, and with it the cloud level, should lower with a decrease in H1. This is shown in figure 5. It is seen that although  $H_1$  and  $H_{c1}$  have the same mean value (1,800 ft),  $H_1$  has a greater range of variation than Hcl. From figure 4 we also see that the lowest inversions occur at about 85 to 90 percent relative humidity, while the highest are at about 100 percent. The cloud height generally occurs at about the 95 percent relative humidity level. Thus the moisture content of the stirred layer does not vary enough with height of the inversion to keep the top of the stirred layer at 95 to 100 percent relative humidity. Instead, the highest inversion occurs at the top of a layer of scattered, flat cumuli, while the lowest occurs in the large, perfectly clear (of low clouds) areas between large, isolated cumulonimbi, and below the general cloud bases. The relation works both ways; under showery conditions moisture is added to the stirred layer by falling rain as well as by evaporation from the sea surface. This lowers the cloud level, but at the same time the descending dry currents must reach lower in order to compensate for the larger ascending moist currents, lowering the H1 inversion between clouds. For example, on May 14, when showery weather conditions prevailed in the Saipan area (fig. 2 and table 1), the mixing ratio in the stirred layer was above average and the cloud base below average. This was the time when the lowest inversion was observed between the large clouds, where large areas entirely free of clouds were present. However, the inversion will not always be lower than the lowest cloud bases under such conditions. Local ceilings in showers may be considerably lower (as on May 4). On the other hand, when the inversion was relatively high, many small cumulus clouds were observed, instead of a few large ones. To summarize, the inversion height and cloud height will vary in the same sense for the following reasons:

<sup>(1)</sup> The lower the inversion, the higher the mixing ratio in the stirred layer and the lower the condensation level.

- (2) The lower the condensation level, the lower must the dry downward currents extend to compensate for the moist upward currents.
- (3) The addition of moisture to the stirred layer by showers, lowering the cloud base, occurs under conditions favoring powerful local subsidence between clouds, lowering the inversion.

Moisture Discontinuity. The strength of the moisture discontinuity at  $H_1$  is determined by three variables:

- (1) The mixing ratio of the stirred layer  $(\overline{w}_{st})$ . This quantity varied through a total range of 2.4 g/kg (table 1). A rough estimate of  $\overline{w}_{st}$  can be obtained from the cloud height (except in showers) by assuming that it is the 95 percent relative humidity level at a potential temperature of 299.5°K (fig. 4).
- (2) The mixing ratio in the layer above the transition zone. The mean mixing ratio in the layer from 2,500 to 4,000 ft ( $\overline{w}_{25-40}$  in table 1) is used as a measure of this quantity. The range of variation is 5.4 g/kg, or more than twice the variation in the stirred layer. The average value of  $\overline{w}_{25-40}$  - $\overline{w}_{st}$  is 3.9. Only about half the moisture transition takes place in the inversion layer ( $\Delta w_1$  = 2.0). It is seen from figure 6 that  $\Delta w_1$  can be estimated roughly from a knowledge of  $\overline{w}_{25-40}$  alone. A correction can be applied for the deviation of  $\overline{w}_{st}$  from the mean. The variation of  $\overline{w}_{25-40}$  with time is shown in figure 2 for both airplane and radiosonde observations. Excluding measurements made in clouds, the airplane and radiosonde values agree quite well. Values of  $\overline{w}_{25-40}$  vary with the degree of convective activity, values of less than 12 being associated with prevailing flat cumulus clouds and values over 14 occurring in showery weather. It is possible then to obtain a preliminary estimate of w<sub>1</sub> without making a detailed sounding. Since the temperature discontinuity is very small, it is seen from the definition of M (see footnote, p. 4) that  $\Delta M_1 - 5\Delta h_1$  will depend mainly upon  $\Delta w_1$ . Figure 7 shows  $\Delta M_1$  -  $5\Delta h_1$  plotted against  $\Delta w_1$ . The line  $\Delta M_1$  -  $5\Delta h_1$ =  $-7\Delta w_1$  - 1 can be used to give an approximation to  $\Delta M_1$  -  $5\Delta h_1$ .
- (3) The depth of the transition layer ( $\Delta h_1$ ). In the present series of measurements, the transition layer varied in thickness from 100 to 800 ft, with an average value of 300 ft. This is the most difficult of the factors to take into account, since it seems to have little relation to the other atmospheric characteristics observed. One reason for this apparently erratic variation may be the lack of sufficiently closely spaced readings in the vicinity of the transition zone for accurate determination of its depth. It was pointed out above (sec. 4.2) that 55 percent of the measured values depend only on two readings. However, from the plot of  $\Delta h_1$  against  $\Delta w_1$  in figure 8, it is seen that 65 percent of the values of  $\Delta h_1$  are 100 or 200 ft, roughly equal to the altitude interval between readings, but at values of  $\Delta w_1$  of 2 g/kg or greater, larger values of  $\Delta h_1$  appear. Within the accuracy of measurement,  $\Delta h_1$  = 125  $\Delta w_1$  seems a fair approximation. Although the points are too scattered to warrant any quantitative conclusions, it appears that there is a limiting vertical gradient of moisture in the inversion, the greater decreases of moisture requiring deeper transition layers. This fact would be useful in estimating  $\Delta M_1$ , the modified index inversion, using an estimated  $\Delta M_1$  -  $5\Delta h_1$  obtained as indicated in (2) above. In fact, for  $\Delta w_1 < 2$ ,

for practical purposes (within the limits of our measurements)  $\Delta h_1$  is constant;  $\Delta M_1$  can be estimated directly from  $\Delta w_1$ , as shown in figure 9. More accurate measurements will be required before a definite relation can be found between  $\Delta h_1$  and other variables. For instance, it is likely that  $\Delta h_1$  will vary considerably with different convective patterns. The partial stirring that occurs in a layer of fractocumulus clouds may act to spread out the discontinuity, while the sinking currents between towering cumulus or cumulonimbus clouds may tend to concentrate the transition in a narrow zone. It would follow then that  $\Delta w_1$  is determined mainly by large-scale subsidence and convergence associated with varying synoptic situations, while  $\Delta h_1$  is a function of local subsidence associated with individual convective cells. Figure 10 shows an example of a sounding with a very moist stirred layer, low cloud base and small  $\Delta w_1$ , and one with a dry stirred layer, high cloud base and large  $\Delta w_1$ .

#### 5. HIGHER INVERSIONS

## 5.1 Theory

It is well known that in the trade-wind current, a temperature inversion with a decrease of mixing ratio commonly occurs at some level between about 4,000 and 10,000 ft, the height varying with the synoptic situation. This inversion is known as the "trade inversion" or the "top of the moist layer." It is usually the upper limit of general cumulus development, although individual towering cumulus or cumulonimbus clouds will sometimes penetrate it. During periods of widespread shower activity the stable layer may disappear temporarily. Its height is in the range of theoretical values of the top of the layer of turbulent influence given in table 5.

#### 5.2 Measurements

Seven of the 12 airplane soundings reaching 8,000 ft showed a stable layer based at some altitude between 3,500 and 7,000 ft, the average altitude being 5,000 ft. Of twenty-one 12-hourly radiosonde records for the period from May 6 to May 16, 16 show a relatively stable layer, also appearing at an average altitude (H2) of 5,000 ft. As shown by the radiosondes, the average vertical extent of the inversion is 1,900 ft, the average temperature lapse is 0.9°C, and the average mixing ratio lapse is 4.6 g/kg (fig. 1 and table 2). Approximate readings taken from plotted soundings for the period April 28 to May 6 show the same pattern, but with somewhat higher values of H2. This inversion fluctuates with the weather (fig. 2), generally following the general cumulus tops and disappearing in periods of abnormal instability. The airplane soundings and radiosondes do not agree well on either the height or the intensity of the inversion, but this may be due to the fact that the airplane soundings were made at a different time and up to 150 mi distant from the radiosondes. The H2 inversion showed considerable changes in these distances. The strongest inversion was observed by the airplane 50 mi east of Saipan at 1123 GMT on May 9, and 50 mi farther east no inversion could be found. The Saipan radiosondes showed a stable layer on this occasion, the top agreeing well with that measured by the airplane 50 mi east, but the base appearing considerably lower on the radiosonde. In no case was a moisture discontinuity found of sufficient intensity to form a duct (M-inversion). However, neither the radiosondes nor the airplane soundings in this altitude range were

sufficiently detailed to be conclusive. It is possible that the normal cumulus deck is a result of mechanical stirring, and the  $\rm H_2$  is the limit of frictional influence. This would help explain the otherwise puzzling fact that temperatures measured within cumulus clouds were always lower than those measured in the clear environment. However, the values of  $\rm H_2$  agree with theoretical values of the height of the layer of turbulent influence (based on the 4,000-ft wind at Saipan) only in order of magnitude; their variations show no apparent correlation. Our measurements are insufficient to justify drawing any conclusions on this point.

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Table 1. -- Summary of airplane observations

												•		is.				
Weather (soundings)	Through layer of scatt, cum.				•	,	·		ì	ċ	0	Clear. In cum. clouds, light rain in top.		Clear. In or under clouds.				
Wear (sour	Throu	Clear	Clear	5	Clear	Clear,	Clear	Clear	Clear	Clear	Clear,		Clear,	Clear. In or	Clear	Clear	Clear,	t., Clear,
Weather (general)	Few cum.	Clear,	Clear,		to 1,000 it.	2/10 cum., cum. nimb. 80 mi S.	2/10 cum., line of cum. nimb. 80 mi S.	Many scatt. show., broken cum., few cum. nimb.	6/10 cum. tops 7,500 ft, line of cum nimb S.	10/10 altostrat., 2/10 small cum.	10/10 altostrat., 2/10 small cum.	Scatt. cum. to 5,000 ft, few to 7,000 ft.	Scatt. cum.	3/10 cum. to 4,000 ft, few tops to	Scatt. cum.	Few cum.	Few cum.	Few patches altostrat., no low cloud, Cle
W25-40	12.0	13.7	Too few readings	12.9		12.9	13.4	15.0	14.5	13.3	12.7	14.0 }	14.1	13.4	12.0	13.4	10.9	12.0
ΔT <sub>20-40</sub>	-2.5	9.4-	Too few	-4.2		-3.6	-3.5	-3.6	-3.3	-3.3	-2.8	-3.8	-5.0	-2.4	-2.9	-4.1	-3.0	-3.9
v20	03	03	02	05		10	10	17	17	16	16	12	12	12	12	80	80	80
Γ <sub>M</sub> ∇	-10	80	+ 3	+ 5		+ 5	9 -	+ 1	+ 1	-10	7 -	7	1	0 1	1	- 1	-10	7 +
Δw <sub>1</sub>	2.5	1.6	0.7	0.5		1.0	2.9	1.9	1.2	2.9	1.1	0.7		1.2	1.9	0.7	2.1	2.6
$^{\Delta T_1}$	0	+0.5	0	0		-0.5	0	-0.3	-0.1	+0.1	+0.3	+0.1		+0.2	not enough readings	+0.2	+0.2	-0.5
$^{\Delta h_1}$	1	1	2	2	(	7	С.	m	2	7	7	н 1	8	1 2	not	П	1	5
H	18	14	16	16		14	16	12	16	15	14	22	ading	18	20	15	15	13
H <sub>c1</sub>	17	1	1	22	(	19	17	6	16	11	11	21	- Not enough readings	21	21	18	1	1
ΔMs	45	94	94	53		45	42	36	37	32	37	45	t eno	43	47	04	47	20
w st	16.0	16.2	16.2	15.7	,	16.6	17.2	18.1	17.9	17.5	17.3	17.2	No No	17.0	16.3	17.3	16.4	16.0
S S	22.0	22.2	22.2	23.3	0	6.77	22.9	23.1	23.1	22.2	22.4	23.5		23.0	23.0	22.6	23.0	23.1
L s	26.9	27.1	27.1	27.9	1	9.17	27.6	27.8	27.8	27.1	27.2	28.0		27.7	27.7	27.4	27.7	27.8
e st	298.7	298.9	298.7	299.7	000	4.667	299.4	299.6	299.6	298.9	299.0	299.8		299.5	299.5	299.2	299.5	299.6
Location	Just NE Saipan	100 mi NE	100 mt NE	Farallon I.		90 mi N	Farallon I.	100 mi N	100 mi N	100 mi N	100 mi N	20 mi NE	20 mi NE	} 40 mi NE	Near Saipan	50 mi E	100 mi E	150 mi E
Local	1046*	1132	1249	1518	17.13	1413	1506	1402	1501	1416	1511	1348*	1520	1345*	1520	1123	1254	1415
Date	Apr. 29	29	29	30	May	7	က	4	4	9	9	~ ~	7	∞ ∞	8	6	6	6

Table 1. -- Summary of airplane observations (continued)

L	Location	θ st	H	» S	w st	ΔMS	H <sub>c1</sub>	Н1 /	Δh <sub>1</sub>	ΔT <sub>1</sub> ′	$^{\Delta w_1}$	ν L <sub>M</sub> Ω	v20	<sup>v</sup> 20-40	W24-40	Weather (general)	Weather (soundings)
15(	150-20 mi F	E 299.6	27.8	23.1	16.2	65	17	17	П	0	3.6	-20	80	-3.1	9.6	Few patches altostrat., few cum.	Clear.
6	35 mi E	299.6	27.8	23.1	17.6	40	17	26*	2	+0.3	2.4	- 2	16	-2.3	11.6	4/10 cum. tops to 2,500 ft.	Through area of scatt. cum.
2	20 mi E	299.6	27.8	23.1	16.2	65	17	16	2	+0.1	5.3	-11	16	-3.7	10.8	4/10 cum.	Clear area.
2	25 mi E	299.7	27.9	23.3	16.3	65	1	19	9	9.0-	3.5	-11	12	-2.6	11.7	Scatt. cum.	Clear.
25	25-65 mi E	299.6	27.8	23.1	16.2	67	19	18	2	-0.2	4.4	∞ 1	12	-2.6	11.4	Scatt. cum.	Clear.
7	.70 mi E	299.6	27.8	23.1	16.8	45	20	18	8	-1.0	8.4	- 2	12	-2.7	11.2	Scatt, cum.	Clear.
70	70-10 mi E	299.6	27.8	23.1	16.5	47	20	23+	ПП	0-0.2	1.9	- 1	12	-3.0	11.3	Scatt. cum. tops to 2,800 ft., few to 9,000 ft.	Clear.
(1	20 mi E	299.6	27.8	23.1	17.5	41	13	118	1   1	10.1	1.9	+ 1 + 1	19	-3.9	13.9	3/10 cum. to 11,000 ft, cum. nimb. S.	Clear spot
7	40 mi E	299.4	27.6	22.9	17.9	36	15	17/10	2   2	0.3	0.5	7 + 4	19	-3.8	14.8	2/10 cum to 9,000 ft in being, cum. nimb. E.	Clear area.
	70 mi E		Points	too sc	too scattered	-	15	11	ПΠ	010	0.8	- 4	19	-4.1	14.5	5/10 cum. to 8,000 ft.	Clear.
	50 mi E	299.8	28.0	23.5	16.7	8 7	20	23	2	+0.2	3.0	9 -	12	-2.6	12.8	3/10 small cum., few tops to 5,000 ft.	Clear spot.
	50 mi E	299.8	28.0	23.5	16.7	84	22 {	22	n ا	9.0-	2.7	+ 1	12	-3.1	13.3	3/10 small cum., few tops to 5,000 ft.	Clear. In or under clouds.
	50 mi E	299.8	28.0	23.5	16.5	64	22	25	1	+0.1	1.3	7 -	12	-2.4	13.2	3/10 small sum., few tops to 5,000 ft.	Clear.
		299.5	27.7	23.0	16.8	77	17.5	17.1	2.4	-0.1	2.0	8	1	-3.5	12.9		
		299.8	28.0	23.5	18.1	53	22	26	80	+0.5	5.3	+ 7	1	-5.1	15.0		
		298.7	26.9	22.0	15.7	32	6	10	1	-1.0	7.0	-20	1	-2.3	9.6		

<sup>\*</sup> Observation through clouds. + The two transition layers, both heights + and corresponding  $\Delta h_1$ ,  $\Delta r_1$ ,  $\Delta w$ , and  $\Delta M_1$  are given, separated by a bar (-).

Table 2. -- Summary of radiosonde observations

v <sub>40</sub> (mi/h)	90	07	03	04	02	05	05	07	80	10	12	16	21	16	12	19	19	15	14	13
<sup>w</sup> 100 (g/kg)																	7.6	0.4	9.7	4.2
T <sub>100</sub> (°C)																	14.3	11.1	11.7	10.4
dt/dh <sub>100</sub> (°C/1,000 ft)																	-2.4	-2.4	-0.7	-2.2
W25-40 (g/kg)																	19.3	6.6	12.5	12.8
ΔT <sub>20</sub> -40 (°C)																	-2.1	-1.7	-2.9	-3.7
Δw <sub>2</sub> (g/kg)								Approximate values									-3.8	-2.2	-5.4	9.0+
ΔT <sub>2</sub> (°C)								Approxi						_			6.0+	+0.3	+3.0	6.0+
∆h <sub>2</sub> (ft)	1,200	1,700	3,400	2,500	700	2,000	2,100	1	3,700	1	700	1,700	1,300	009		1	1,000	1,000	2,000	800
H <sub>2</sub> (ft)	4,800	7,600	4,400	7,500	007,6	7,600	7,500	1	2,900	1	5,700	8,200	7,900	2,600	1	1	2,900	2,400	000,9	2,800
Local	2300	1100	2300	1100	2300	1100	2300	1100	2300	1100	2300	1100	2300	1100	2 300	1100	2300	1100	2300	1100
Date	April 28	" 29	" 29	" 30	" 30	May 1	" 1	" 2	2	3	3	7	7	5	1 5	9	9	7	7	∞ =

Table 2. -- Summary of radiosonde observations (continued)

Date	Local	H <sub>2</sub> (ft)	Δh <sub>2</sub> (ft)	ΔT <sub>2</sub> (°C)	<sup>∆w</sup> <sub>2</sub> (g/kg)	ΔT <sub>20-40</sub> (°C)	W25-40 (g/kg)	dt/dh <sub>100</sub> (°C/1,000 ft)	T100 (°C)	<sup>w</sup> 100 (g/kg)	V40 (mi/h)
. 00	2300	5,000	1,000	0	8.0-	-4.2	11.2	-1.6	8.7	4.0	11
6	1100	2,000	3,500	-3.2	-10.1	-2.8	12.3	-2.1	12.5	1	12
6	2300	1	1	1	1	-3.7	13.6	-1.8	8.1	4.3	04
10	1100	1	1	1	1	-3.4	15.2	-1.7	14.4	7.0	18
10	2300	}	-	1	1	-4.5	15.0	-2.0	8.1	7.3	18
11	1100	4,500	700	-0.5	-1.0	-3.6	11.0	-1.7	12.9	7.5	26
11	2300	4,600	800	+0.7	-3.7	-2.0	19.1	-3.1	14.1	5.7	18
12	1100	4,500	2,300	+1.5	9.9-	-4.2	11.1	-2.3	13.2	2.1	16
12	2300	5,000	1,700	4.0-	-7.0	-4.3	13.8	-2.1	10.2	2.2	14
13	1100	4,500	800	0	-1.2	-3.4	12.1	-1.6	10.5	1	08
13	2300	4,000	009	0	-1.0	-2.4	11.0	-1.8	10.0	2.6	18
14	1100	4,700	1	1	1	-3.9	14.9	-1.6	10.2	8.6	24
14	2300	1	1	1	1	-5.0	11.4	-1.8	6.1	8.9	16
15	1100	4,600	2,800	-2.6	-6.5	6.4-	16.8	-2.3	11.1	8.2	15
15	2300	5,500	3,000	-3.3	-8.8	-3.6	14.3	-2.1	10.5	4.0	16
16	1100	1	1	1	1	-3.5	12.7	-1.1	14.1	3.7	17
16	2300	5,100	3,200	-3.9	-7.5	-3.4	13.4	-1.9	8.7	2.1 °	14
Average		5,000	1,900	6.0-	9.4-	-3.5	13.5	-2.0	11.1	5.4	13
Maximum		0000,9	2,000	+1.5	9.0+	-5.0	19.3	-3.1	14.4	9.7	26
Minimum		4,000	009	-3.9	-10.1	-1.7	6.6	-0.7	6.1	2.1	02

(mb) (g/kg)  33.8 21.4 410  34.2 21.6 412  35.0 22.1 415  35.4 22.4 416  35.4 22.9 418  36.6 23.1 419  37.1 23.5 421  37.9 24.0 424  38.4 24.3 426  38.8 24.6 427  39.4 24.5 428  40.4 25.6 432  40.8 25.2 43  41.3 26.1 435	Ts	a S	WS	M * S		1
33.8       21.4       410       4.0         34.2       21.6       412       4.2         34.6       21.8       413       4.4         35.0       22.1       416       4.6         35.4       22.4       416       4.8         35.8       22.6       417       5.0         36.6       23.1       419       5.4         36.6       23.1       421       5.6         37.1       23.5       421       5.6         37.9       24.0       424       6.0         38.4       24.5       424       6.0         38.8       24.6       427       6.6         39.9       25.2       430       6.8         40.4       25.6       430       6.8         40.8       25.8       434       7.0         41.3       26.4       437       7.6         41.7       26.4       437       7.6	(0,	(qm)	(g/kg)		S S	ΩM S
34.2       21.6       412       4.2         34.6       21.8       413       4.4         35.0       22.1       415       4.6         35.4       22.4       416       4.8         35.8       22.6       417       5.0         36.2       22.9       418       5.2         36.6       23.1       419       5.4         37.1       23.5       421       5.6         37.6       23.8       424       6.0         37.9       24.0       426       6.0         38.4       24.5       426       6.2         39.4       24.9       428       6.6         40.4       25.6       436       7.0         40.8       25.8       434       7.2         41.3       26.1       435       7.4         41.7       26.4       437       7.6         7.8       41.7       437       7.6	5.4	33.8	21.4	410	4.0	28
34.6       21.8       413       4.4         35.0       22.1       415       4.6         35.4       22.4       416       4.8         35.8       22.6       417       5.0         36.2       22.9       418       5.2         36.6       23.1       421       5.4         37.1       23.5       421       5.6         37.9       24.0       424       6.0         38.4       24.5       426       6.2         38.8       24.6       427       6.4         39.4       24.9       428       6.6         40.4       25.6       430       6.8         40.8       25.8       434       7.2         41.3       26.1       437       7.6         41.7       26.4       437       7.6	9.9	34.2	21.6	412	4.2	30
35.0       22.1       415       4.6         35.4       22.4       416       4.8         35.8       22.6       418       5.0         36.2       22.9       418       5.2         36.6       23.1       421       5.4         37.1       23.5       421       5.4         37.6       23.8       423       5.8         37.9       24.0       424       6.0         38.8       24.6       427       6.4         39.4       24.9       428       6.6         40.4       25.2       430       6.8         40.4       25.6       434       7.2         41.3       26.1       435       7.4         41.7       26.4       437       7.6         7.8       7.8       7.8	8.9	34.6	21.8	413	4.4	31
35.4       22.4       416       4.8         35.8       22.6       417       5.0         36.2       22.9       418       5.0         36.6       23.1       419       5.4         37.1       23.5       421       5.6         37.6       23.8       423       5.8         37.9       24.0       424       6.0         38.4       24.5       424       6.2         39.4       24.9       427       6.4         39.4       24.9       428       6.6         40.4       25.2       430       6.8         40.8       25.8       434       7.2         41.3       26.1       435       7.4         41.7       26.4       437       7.6         7.8       7.8       7.8	0.7	35.0	22.1	415	4.6	33
35.8       22.6       417       5.0         36.2       22.9       418       5.2         36.6       23.1       419       5.4         37.1       23.5       421       5.6         37.9       24.0       424       6.0         38.4       24.3       426       6.2         38.8       24.6       427       6.4         39.4       24.9       428       6.4         39.9       25.2       430       6.8         40.4       25.6       432       7.0         40.8       25.8       434       7.2         41.3       26.1       435       7.4         41.7       26.4       437       7.6	7.2	35.4	22.4	416	4.8	34
36.2       22.9       418       5.2         36.6       23.1       419       5.4         37.1       23.5       421       5.6         37.6       23.8       423       5.8         37.9       24.0       424       6.0         38.4       24.5       426       6.2         38.8       24.6       427       6.4         39.4       24.9       428       6.6         40.4       25.2       430       6.8         40.8       25.6       432       7.0         40.8       25.8       434       7.2         41.3       26.1       435       7.4         41.7       26.4       437       7.6	7.4	35.8	22.6	417	5.0	35
36.6       23.1       419       5.4         37.1       23.5       421       5.6         37.6       23.8       423       5.8         37.9       24.0       424       6.0         38.8       24.6       427       6.4         39.4       24.9       428       6.4         39.9       25.2       430       6.8         40.4       25.6       432       7.0         40.8       25.8       434       7.2         41.7       26.4       437       7.6         41.7       26.4       437       7.6	9.7	36.2	22.9	418	5.2	37
37.1       23.5       421       5.6         37.6       23.8       423       5.8         37.9       24.0       424       6.0         38.4       24.3       426       6.2         38.8       24.6       427       6.4         39.4       24.9       428       6.6         39.9       25.2       430       6.8         40.4       25.6       432       7.0         40.8       25.8       434       7.2         41.3       26.4       437       7.6         41.7       26.4       437       7.6	8.7	36.6	23.1	419	5.4	39
37.6       23.8       423       5.8         37.9       24.0       424       6.0         38.4       24.3       426       6.2         38.8       24.6       427       6.4         39.4       24.9       428       6.6         39.9       25.2       430       6.8         40.4       25.6       432       7.0         40.8       25.8       434       7.2         41.3       26.1       435       7.4         41.7       26.4       437       7.6         7.8       7.8	3.0	37.1	23.5	421	5.6	41
37.9       24.0       424       6.0         38.4       24.3       426       6.2         38.8       24.6       427       6.4         39.4       24.9       428       6.6         39.9       25.2       430       6.8         40.4       25.6       432       7.0         40.8       25.8       434       7.2         41.3       26.1       435       7.4         41.7       26.4       437       7.6	3.2	37.6	23.8	423	5.8	42
38.4       24.3       426       6.2         38.8       24.6       427       6.4         39.4       24.9       428       6.6         39.9       25.2       430       6.8         40.4       25.6       432       7.0         40.8       25.8       434       7.2         41.3       26.1       435       7.4         41.7       26.4       437       7.6         7.8       7.8	3.4	37.9	24.0	424	0.9	43
38.8       24.6       427       6.4         39.4       24.9       428       6.6         39.9       25.2       430       6.8         40.4       25.6       432       7.0         40.8       25.8       434       7.2         41.3       26.1       435       7.4         41.7       26.4       437       7.6         7.8       7.8	3.6	38.4	24.3	426	6.2	45
39.4       24.9       428       6.6         39.9       25.2       430       6.8         40.4       25.6       432       7.0         40.8       25.8       434       7.2         41.3       26.1       435       7.4         41.7       26.4       437       7.6         7.8       7.8	8.8	38.8	24.6	427	4.9	97
39.9       25.2       430       6.8         40.4       25.6       432       7.0         40.8       25.8       434       7.2         41.3       26.1       435       7.4         41.7       26.4       437       7.6         7.8       7.8	0.0	39.4	24.9	428	9.9	£7
40.4       25.6       432       7.0         40.8       25.8       434       7.2         41.3       26.1       435       7.4         41.7       26.4       437       7.6         7.8       7.8	9.2	39.9	25.2	430	8.9	48
40.8       25.8       434       7.2         41.3       26.1       435       7.4         41.7       26.4       437       7.6         7.8       7.8	4.6	40.4	25.6	432	7.0	50
41.3     26.1     435     7.4       41.7     26.4     437     7.6       7.8	9.6	8.04	25.8	434	7.2	51
41.7 26.4 437 7.6	8.6	41.3	26.1	4.35	7.4	52
	0.0	41.7	26.4	437	7.6	54
					7.8	55

 $\frac{79}{T_s}$  (1,013 + 4,800  $\frac{e_s}{T_s}$ ) \* × ×

$^{ m VM}_{ m S}$	28	30	31	33	34	35	37	39	41	42	43	45	94	64	48	20	51	52	54	55	57
$^{\Delta W}_{\mathbf{S}}$	4.0	4.2	4.4	9.4	8.4	5.0	5.2	5.4	5.6	5.8	0.9	6.2	7.9	9.9	8.9	7.0	7.2	7.4	7.6	7.8	8.0

Table 5.--Height of the layer of frictional influence (in feet, lat.  $15^{\rm O}{\rm N}$ )

	3,300				7,200	00006	
10.0	3						
	100				11,000	14,000	
)	3,300		3,500	5,300	7,000	8,800	
5.0	100		4,800	7,300	9,700	12,000	
2.0	3,300	1,600	3,200	7,800	007,9	8,000	
	100	2,100	4,300	007,9	8,600	11,000	
1.0	3,300	1,500	3,000	4,500	000,9	7,500	
	100	2,000	4,000	000,9	8,000		
0.5	3,300	1,400	2,900	4,300			
0	100	1,800	3,600	2,400			
р	ď		-				
	>	7	10	15	20	25	

a = height of wind measurement, feet.

b = height of ocean waves, feet.

v = wind velocity, miles per hour.

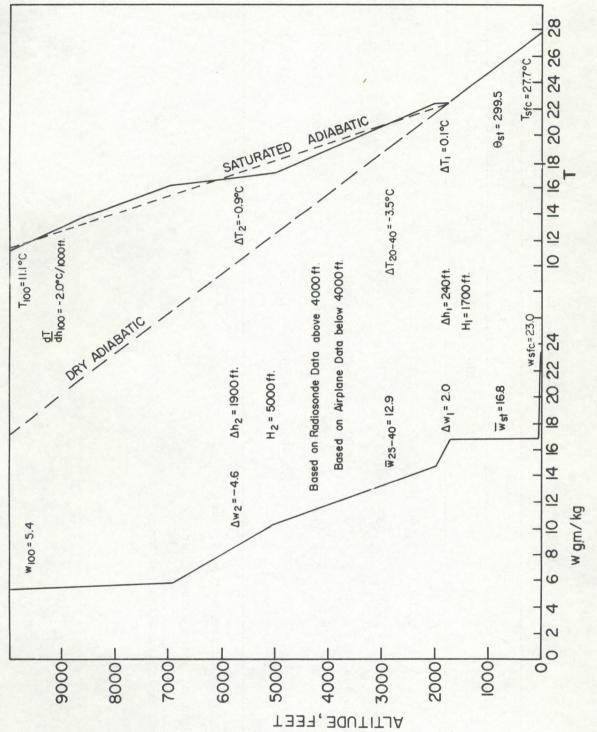


Figure 1.--Average characteristics of the lower atmosphere.

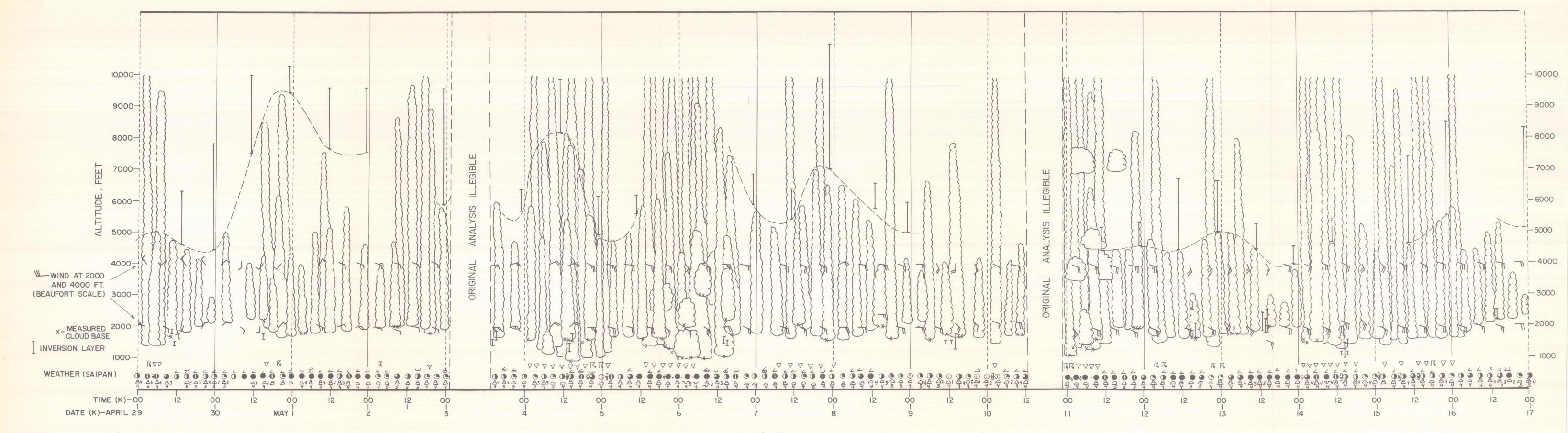
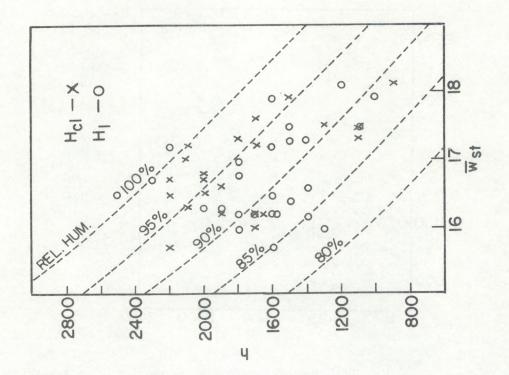
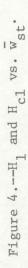


Figure 2.--Time cross section.





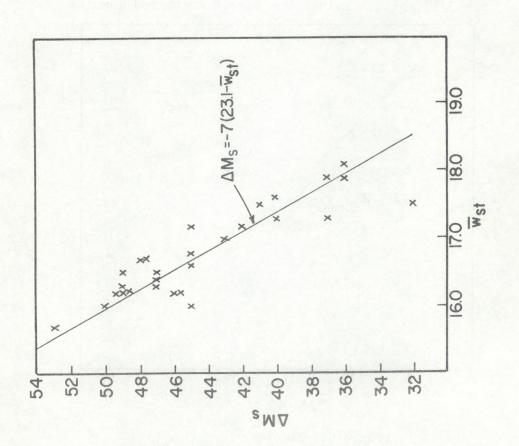


Figure 3.-- AM vs. ws.

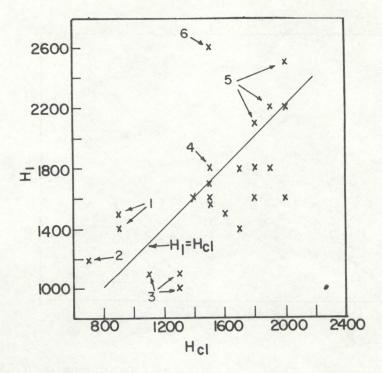


Figure 5.--H $_1$  vs. H $_{c1}$ . 1 - 2/10 small cumulus; 2 - shower; 3 - towering cumulus and cumulonimbus; 4 - through scatter cumulus area; 5 - 3/10 small cumulus; 6 - top of scattered cumulus.

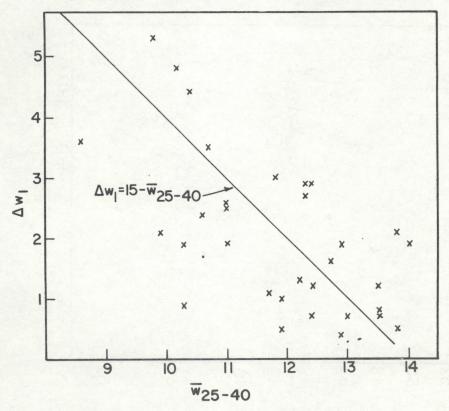


Figure 6.-- $\Delta w_1$  vs.  $w_{25-40}$ .

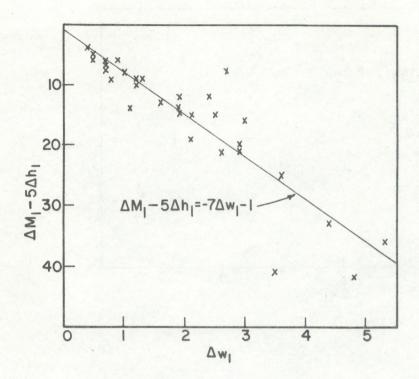


Figure 7.-- $\Delta M_1$ -5 $\Delta h_1$  vs.  $\Delta w_1$ .

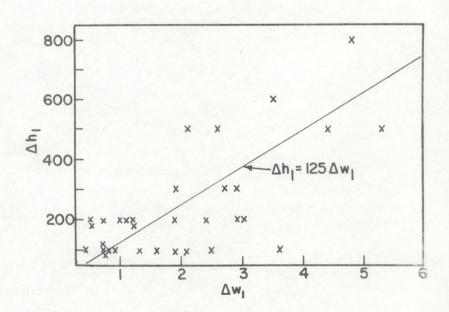


Figure 8.— $\Delta h_1$  vs.  $\Delta w_1$ .

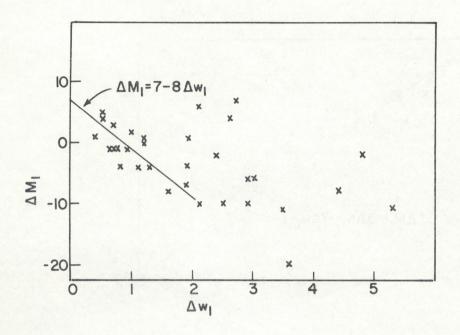


Figure 9.-- $\Delta M_1$  vs.  $\Delta w_1$ .

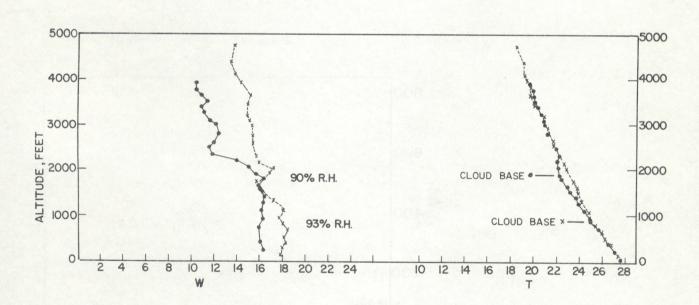


Figure 10.--Two sample soundings.